

# Optimization of Top Coupling Grating for Very Long Wavelength QWIP Based on Surface Plasmon

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**Abstract:** The relative coupling efficiency of two-dimensional (2D) grating based on surface plasmon for very long wavelength quantum well infrared detector is analyzed by using the three-dimensional finite-difference time domain (3D-FDTD) method algorithm. The relative coupling efficiency with respect to the grating parameters, such as grating pitch, duty ratio, and grating thickness, is analyzed. The calculated results show that the relative coupling efficiency would reach the largest value for the 14.5  $\mu\text{m}$  incident infrared light when taking the grating pitch as 4.4  $\mu\text{m}$ , the duty ratio as 0.325, and the grating thickness as 0.07  $\mu\text{m}$ , respectively.

**Keywords:** Very long wavelength; QWIP; surface plasmon; 2D grating

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## 1. Introduction

The very long wavelength infrared (VLWIR) spectral range from 14  $\mu\text{m}$  to 20  $\mu\text{m}$  is of great importance for space applications [1, 2]. Quantum well infrared photodetectors (QWIPs) based on the GaAs/AlGaAs material system have been studied in detail and have already been used in large format focal plane arrays [3–6]. Because of its mature growth and processing technology, QWIPs have been investigated as an alternative for VLWIR detection [7, 8].

However, VLWIR QWIPs have a lower performance than that of HgCdTe detectors and suffer from low response photocurrent, partly

because of the lower coupling efficiency of top metal grating. Therefore, it is quite necessary to improve the performances of VLWIR QWIPs.

Since Ebbesen [9] discovered the interesting extraordinary optical transmission of periodic holes array perforated in the metal film, the surface plasmon (SP) has attracted a lot of research interests. SP has been applied in different kinds of devices, such as semiconductors lasers, quantum dot solar cells, and infrared detectors [10–12]. In the very long wavelength infrared band, the SP propagation length is large enough to effectively reach the entire quantum well region, and the optical loss is relatively small. So if SP is applied in VLWIR QWIP, the coupling efficiency of grating and

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response photocurrent will be improved evidently.

In this paper, the coupling grating based on SP for the VLWIR QWIPs is simulated by the finite-difference time domain method (FDTD). The relative coupling efficiencies with respect to different grating parameters are compared, and the optimal parameters of grating have been obtained.

## 2. Simulation model

The three-dimensional finite-difference time domain method (3D-FDTD) is strictly a numerical algorithm for solving Maxwell's equations. It can be applied to simulate the SP waves and electric field component distribution. The simulated structure is shown in Fig. 1. From the bottom to top, the QWIP is composed of GaAs substrate, *n*-type GaAs bottom contact layer, GaAs/AlGaAs multiple quantum well layer, *n*-type GaAs top contact layer, and grating layer (periodic hole array). The source is a normally incident plane wave. For convenience, the growth direction of the MQW layer is set to *z*-coordinate, the bottom of grating layer is set to  $z=0$ , the device plane is set to *x*-*y* plane, and the central point of *x*-*y* plane is set to  $x=0$ ,  $y=0$ .  $P$  and  $D$  respectively represent the grating pitch and the diameter of the hole. Supposing the light incident from the top, the coupling efficiency of *x*-*y* at *z* point can be expressed as [13]

$$\eta(z) = \frac{\iint E_z^2(x, y, z) dx dy}{\iint E_{in}^2(x, y, z) dx dy} \quad (1)$$

where  $E_{in}$  represents the electric field component of the incident light, and  $E_z$  represents the electric field component along the *z* axis in the *x*-*y* plane.

One attraction is that because of the limitation of computer, all the MQW region is not selected to integration. Accordingly, a reasonable integral area is selected and fixed, so the relative coupling efficiency is obtained. This is only due to the limitations of numerical calculation, but does not affect the results of the physical characteristics of

the performance. In this paper, we fix the integration area as  $9.6 \mu\text{m} \times 9.6\sqrt{3} \mu\text{m}$  in the center of *x*-*y* plane.

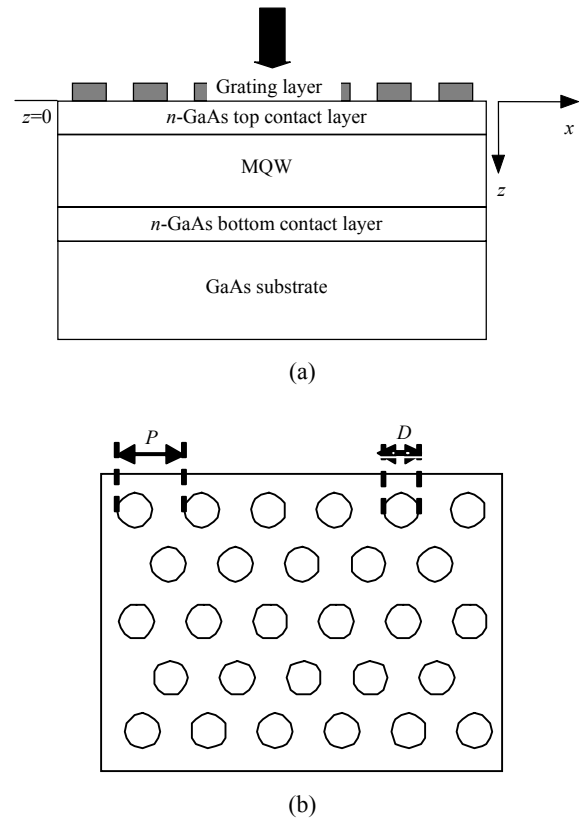


Fig. 1 Modelling structure of VLWIR QWIP: (a) device structure and coordinate direction and (b) structure of periodic hole array.

## 3. Calculation and analysis

Firstly, by setting the incident light as TE mode plane wave ( $E_z = 0$ ) and the central wavelength of incident source as  $14.5 \mu\text{m}$ , the grating parameters as grating pitch  $P = 2.8 \mu\text{m}$ , the diameter of hole  $D = 1.6 \mu\text{m}$ , the thickness of grating layer  $L = 0.08 \mu\text{m}$ , and the  $E_z$  field in *x*-*y* plane are calculated by FDTD. The  $E_z$  distribution at  $z = 0.11 \mu\text{m}$  is illustrated in Fig. 2. As can be seen from Fig. 2, the direction of infrared light propagation has been changed obviously, and  $E_z$  is concentrated on the position in correspondence with the grating holes.

Further calculation shows that the intensity of the light in different *x*-*y* planes is decreased with an increase in *z*, which follows the exponential law, as

shown in Fig. 3. In other words, it can be concluded that the farther away from the grating is, the lower intensity of light in  $x$ - $y$  plane is. It also fits well with the propagation properties of SP wave. So it can be proved that  $E_z$  in the  $x$ - $y$  plane is indeed excited by SP.

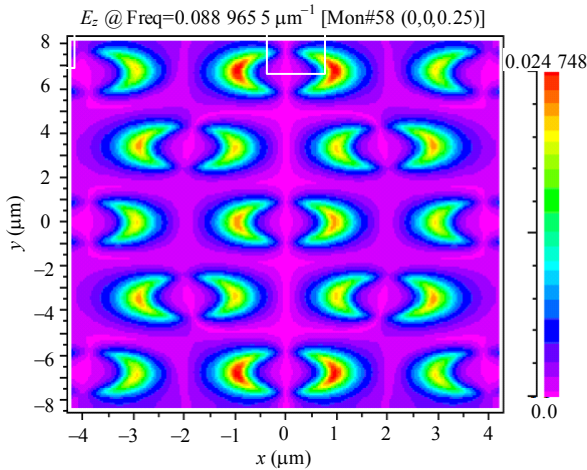


Fig. 2 Distribution of  $E_z$  at  $z=0.11 \mu\text{m}$   $x$ - $y$  plane.

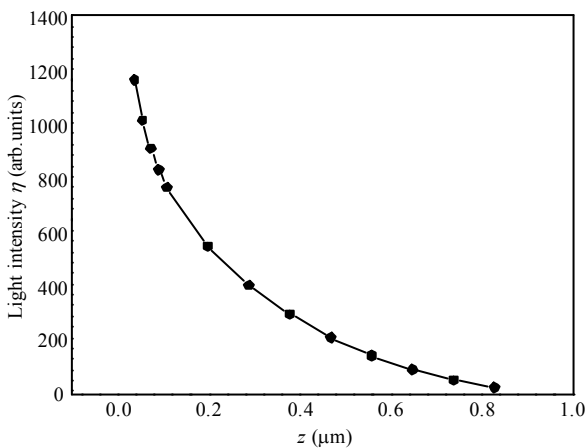


Fig. 3 Distribution of  $E_z$  at different  $x$ - $y$  planes.

Secondly, in order to obtain the more accurate results, the relative coupling efficiency of grating is calculated by (1) in the fixed integral area which is described above. Figure 4 shows the relative coupling efficiency with respect to the grating pitch. It can be seen that the grating coupling efficiency reaches the maximum when the grating pitch is  $4.4 \mu\text{m}$ . This result is in agreement with the grating equation.

And then, by taking the grating pitch as

$P = 4.4 \mu\text{m}$ , the relative coupling efficiency is calculated when the duty ratio  $D/P$  is changed. The calculated results are shown in Fig. 5. It shows that the peak value of relative coupling efficiency is achieved when the duty ratio is taken as 0.325.

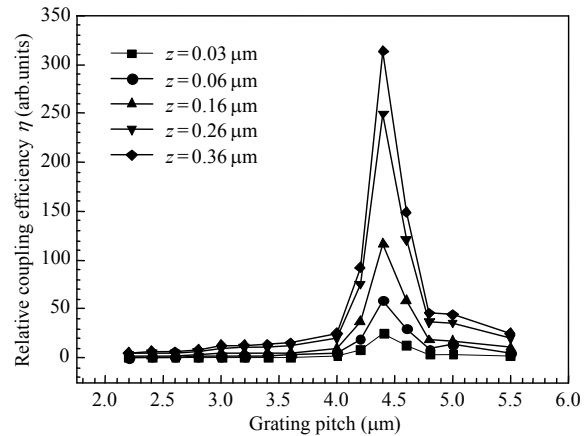


Fig. 4 Relative coupling efficiency with respect to grating pitch.

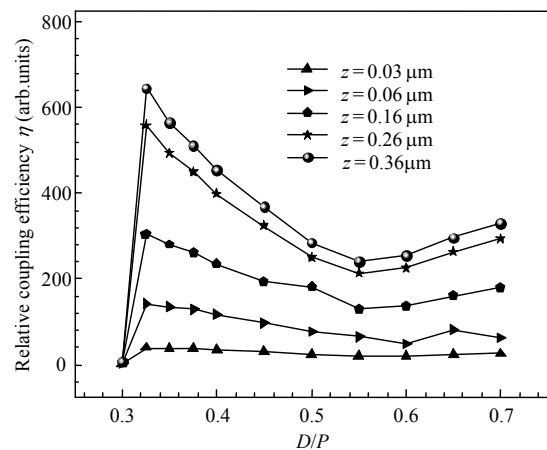


Fig. 5 Relative coupling efficiency with respect to duty ratio  $D/P$ .

Then, by taking duty ratio as  $D/P=0.325$ , the relative coupling efficiency is calculated with respect to the grating thickness. The calculated results are shown in Fig. 6. It can be concluded that the largest relative coupling efficiency will be obtained when the grating thickness is  $0.07 \mu\text{m}$ .

Finally, the optimized parameters of coupling grating for  $15.4 \mu\text{m}$  input infrared light is obtained, which is illustrated as the grating pitch  $4.4 \mu\text{m}$ , the duty ratio 0.325, and the grating thickness  $0.07 \mu\text{m}$ .

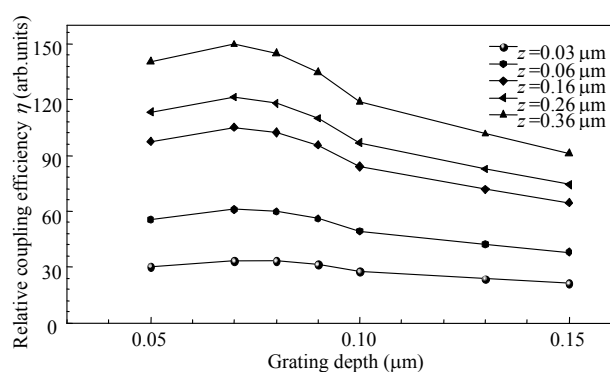


Fig. 6 Relative coupling efficiency with respect to grating thickness.

#### 4. Conclusions

In conclusion, the relative coupling efficiency of top 2D metal coupling grating based on SP for the VLWIR QWIP is calculated by FDTD. The optimized parameters grating is obtained by maximizing the coupling efficiency for different grating parameters. This work is beneficial to enhancing the performance of the very long wavelength QWIP focal plane array devices.

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