

Investigation Into Vibration Characteristic in Vibrothermography

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Abstract: Vibration characteristic plays an important role in vibrothermography, which directly affects the heating during the test. In this work, involving all the contacts in the vibrothermography, the “double-mass-three-spring” model is established to explore the vibration characteristic. The obtained results show that ultrasonic gun vibrates at fundamental frequency (FF), while the specimen vibrates at multi-frequencies including FF, 2FF, 3FF, and 4FF, which is validated through experimental investigation results. Additionally, the model proposed in this work reveals a high order harmonics in the vibrothermography test and makes the specimen conduct the steady vibration, which indicates that the model is closer to the practical equipment and can ensure the heating efficiency induced by vibration of specimen to improve the detection capability.

Keywords: Vibrothermography; vibration characteristic; “double-mass-three-spring” model

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1. Introduction

Vibrothermography [1, 2], also called as thermosonics, ultrasonic infrared thermography, and acoustic thermography, etc., is viewed as a promising active thermal nondestructive method and attracts extensive attention due to its advantages of easy operation, high efficiency, damage selective imaging, clear visualization, and great adaptability to complex structures, etc., which is suitable for crack detection in the materials. During the vibrothermography test, the ultrasonic generator releases ultrasonic waves into the object, resulting in the ultrasonic vibration of the object. If there is a crack in the object, the dissipative phenomena, such as friction between the faces of crack, will transfer

vibrational energy to heat. In this case, we can use an infrared camera to image the heat effect and realize the crack detection. From the process of vibrothermography, it can be known that the principle of vibrothermography mainly contains three aspects: ultrasonic vibration, vibration induced heat, and infrared imaging, among which the ultrasonic vibration is the basis for the latter two and becomes a critical topic of active discussion.

Han *et al.* [3, 4] first found out the “acoustic chaos” phenomenon, i.e., the presence of multi-frequencies in the vibrational spectrum of specimen that was stimulated by ultrasonic wave with a single frequency and pointed out this phenomenon could enhance the heating effect. Afterwards, both Sovodov [5] and Han [6] started to

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explore the generation mechanism of nonlinear vibration in the vibrothermography test. The former pointed out that the nonlinear vibration was caused by the crack induced material nonlinearity, while the latter thought that the nonlinear vibration existed during the vibrothermography test whether there was a crack or not in the specimen, which was validated a “single-mass” model that supposed the ultrasonic horn as a mass whose length varied harmonically. But, they didn’t consider the vibration of specimen. Involving the vibration of specimen, Zheng *et al.* [7] proposed a “double-mass-double-spring” model for the generation of nonlinear vibration in vibrothermography, in which the ultrasonic horn and the specimen were viewed as a “contact-collision” particle pair. The obtained results illustrate the specimen motion stimulated by the ultrasonic horn and the generation mechanism of nonlinear vibration. On this basis, Chen *et al.* [8] investigated the nonlinear vibration in the metal plate stimulated by high-power ultrasonic, which pointed out the main reason for generating the nonlinear vibration was the intermittent contact-collision between the ultrasonic horn and plate. Additionally, considering the inevitable energy loss, Feng *et al.* [9] proposed a mechanical model based on the momentum conservation theorem and investigated the effect of engagement force on vibration characteristics. The obtained results show that the relationship between the engagement force and harmonic order can be described with hyperbola. Tian *et al.* [10] utilized the finite element method to improve the simulation model to investigate the effect of nonlinear vibration on the detection results. The obtained results show that the generation of nonlinear vibration can remove the standing wave and improve the heating efficiency. Totally, the above literatures available have shown that nonlinear vibrations, including harmonics and acoustic chaos, exist unavoidably in the vibrothermography test, which can facilitate the understanding of the vibrothermography

mechanism to some degree. However, the vibration model in the literatures only contains the contacts between the specimen and clamp, and specimen and ultrasonic gun, without considering the contact between the fastening device and ultrasonic gun.

On this account, it is necessary for a further investigation into vibration characteristic in vibrothermography test. In this work, involving all the contacts, a “double-mass-three-spring” model is proposed for the analysis of the vibration characteristic in vibrothermography, which is validated by experiments.

2. Methods section

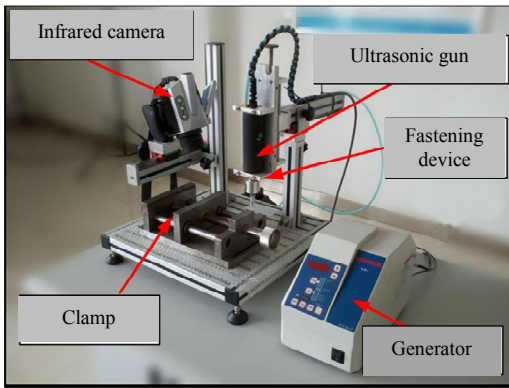
To investigate the vibration characteristic comprehensively, the “double-mass-three-spring” vibration model is first proposed according to the contact state during the vibrothermography test. Then, the steel plate with fatigue crack is used to conduct the experiment for validating the proposed model.

2.1 “Double-mass-three-spring” model

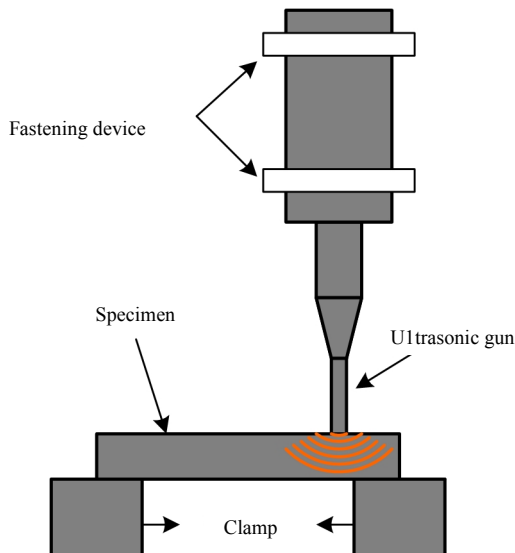
Actually, the ultrasonic gun is generally fixed by a fastening device to facilitate to stimulate the specimen during the vibrothermography test, in this case, the two ends of ultrasonic gun are both restrictive, not a side free, the other restrictive, as shown in Fig. 1. Thus, the contact between the ultrasonic gun and fastening device should be considered in the analysis of the vibration characteristic.

As shown in Fig. 1, the ultrasonic gun and the specimen are fastened by the fastening device and clamp, respectively. Additionally, the contact force F_0 between the ultrasonic gun and the specimen is determined by the fastening device. During the vibrothermography test, the generator releases sinusoidal ultrasonic wave, in the form of $A\sin(2\pi f)$, into the specimen through the ultrasonic gun to induce the vibration of the specimen. Thus, we can conclude that there are three contacts during the vibrothermography test, i.e., the contact between the

fastening device and ultrasonic gun, ultrasonic gun and specimen, and specimen and clamp. Involving all the contacts, a physical model, as shown in Fig. 2, is established to investigate the vibration characteristic, where the ultrasonic horn is equivalent to a particle M_1 with a displacement of X_1 , the specimen is equivalent to a particle M_2 with a displacement of X_2 , and the above-mentioned contacts are equivalent to the springs with the stiffness coefficients of K_1 , K_2 , and K_3 and damping coefficients of R_1 , R_2 , and R_3 , respectively. It is noted that the spring (K_1 , R_1) is inextensible because the ultrasonic horn and specimen can be separated in the actual vibrothermography test.



(a)



(b)

Fig. 1 Vibrothermography test devices: (a) the actual device photo and (b) the simplified sketch map.

From the physical model in Fig. 2, we can deduce the motion equations of M_1 and M_2 based on the Newton second law.

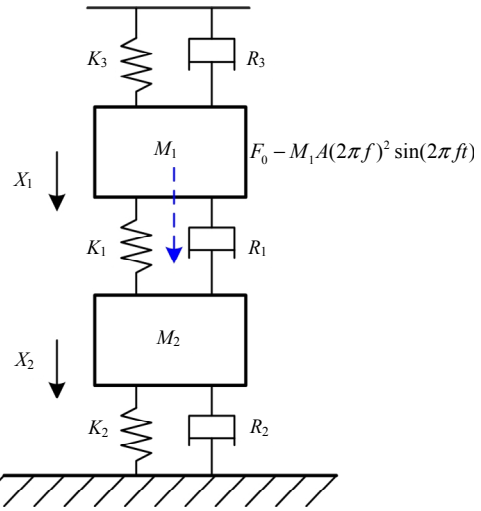


Fig. 2 Physical model of nonlinear vibration.

In the case of $X_1 \geq X_2$, i.e. M_1 is contacted with M_2 , the motion equations can be deduced as follows:

$$\begin{cases} M_1 \ddot{X}_1 = F_0 - M_1 A (2\pi f)^2 \sin(2\pi f t) - K_1 (X_1 - X_2) \\ \quad - R_1 (\dot{X}_1 - \dot{X}_2) - K_3 X_1 - R_3 \dot{X}_1 \\ M_2 \ddot{X}_2 = K_1 (X_1 - X_2) + R_1 (\dot{X}_1 - \dot{X}_2) - K_2 X_2 - R_2 \dot{X}_2 \end{cases} \quad (1)$$

In the case of $X_1 < X_2$, i.e. M_1 is separated from M_2 , the motion equations can be deduced as follows:

$$\begin{cases} M_1 \ddot{X}_1 = F_0 - M_1 A (2\pi f)^2 \sin(2\pi f t) - K_3 X_1 - R_3 \dot{X}_1 \\ M_2 \ddot{X}_2 = -K_2 X_2 - R_2 \dot{X}_2 \end{cases} \quad (2)$$

With the initial condition of $X_1 = X_2 = \dot{X}_1 = \dot{X}_2 = 0$, the corresponding parameters for solving the above equations are listed as: $M_1 = 1$ kg, $M_2 = 0.5$ kg, $F_0 = 200$ N, $A = 70$ μm , $f = 40$ kHz, $K_1 = 10^9$ N/m, $K_2 = 3 \times 10^6$ N/m, $K_3 = 10^{10}$ N/m, $R_1 = 10^5$ N s/m, $R_2 = 100$ N s/m, and $R_3 = 10$ N s/m. It is noted that the parameters used in this work are partly obtained by [7, 9] and partly obtained by experiments.

2.2. Experimental validation

For validating the vibration characteristic of the specimen obtained by the above model, the experimental investigation is carried out in this

section. The specimen studied in the experiment is steel plate with the size of 140 mm × 30 mm × 3 mm, and the ultrasonic stimulation device is produced by Branson company with the type of 2000LPt, which can release the ultrasonic wave with the frequency of 40 kHz to stimulate the steel plate. A laser vibrometer, produced by KEYENCE Company, with the type of LK-G5000, with the accuracy of ±0.02% and the frequency of 392 kHz, is used to measure the displacement of the specimen in the vibrothermography test. The simplified sketch map of the experimental device is shown in Fig. 3.

During the experiment, the continuous ultrasonic wave is released to stimulate the steel plate. When the steel plate reaches to the stable vibration state, the laser vibrometer starts to gather the displacement of measurement point, which is located close to the excitation point between the ultrasonic gun and specimen.

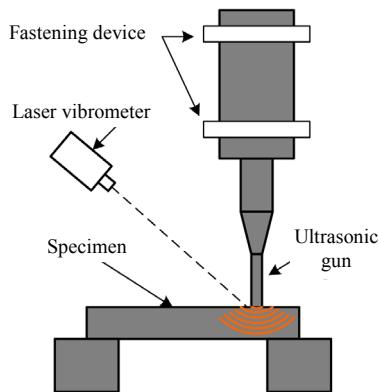


Fig. 3 Simplified sketch map of the experimental device.

3. Results and discussion

Figure 4 shows the vibration displacement of the ultrasonic gun and specimen obtained by the “double-mass-three-spring” model.

As shown in Fig. 4, the ultrasonic gun vibrates in a sinusoidal manner due to the sinusoidal excitation of the generator, which leads to the periodic vibration of specimen. When the ultrasonic gun contacts with the specimen, the displacement of the specimen gradually increases under the action of the spring (K_1, R_1), while the ultrasonic gun separates from the specimen, the displacement of the

specimen gradually decreases under the action of the spring (K_2, R_2). To explore the vibration characteristic of the ultrasonic gun and specimen, the frequency-spectrum analysis is carried out. Figure 5 shows the frequency-spectrum curve of the ultrasonic gun and specimen, where we can know that the ultrasonic gun vibrates at the fundamental frequency (FF) of 40 kHz, while the specimen vibrates at multi-frequencies including FF (40 kHz), 2FF (80 kHz), 3FF (120 kHz), and 4FF (160 kHz).

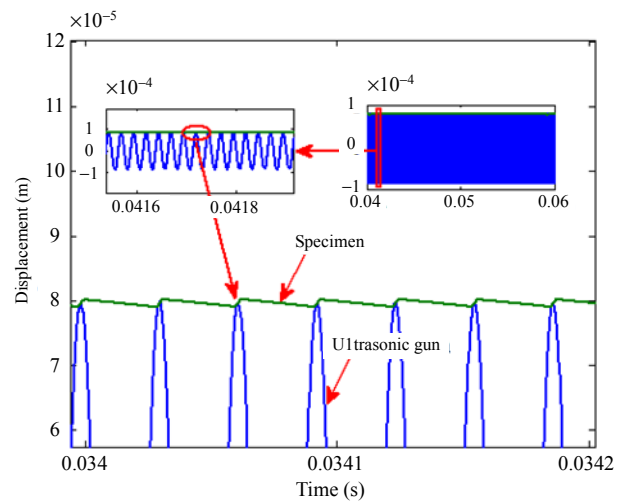


Fig. 4 Vibration displacement of the ultrasonic gun and specimen obtained by the model.

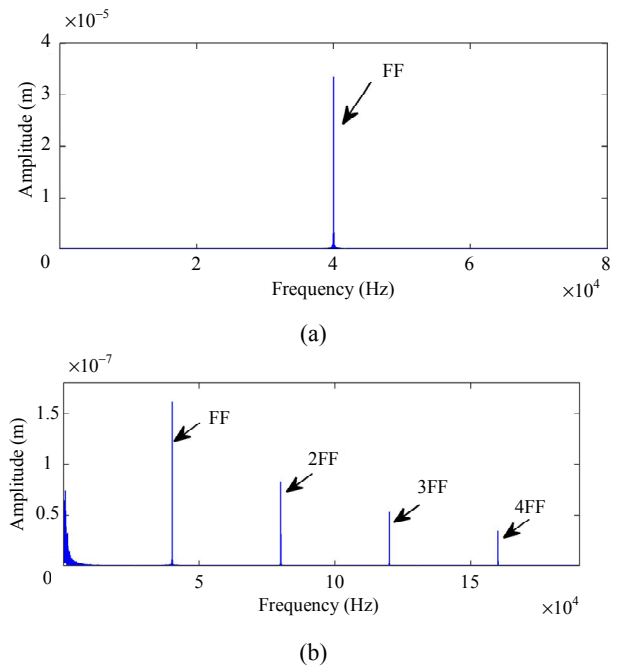


Fig. 5 Frequency-spectrum curve obtained by the model: (a) ultrasonic gun and (b) specimen.

To validate the results obtained by the model, the vibration displacements of 4 measurement points which are randomly selected with the serial number

of 1# – 4# are gathered by using a laser vibrometer. Figure 6 shows the vibration characteristic of 4 measurement points.

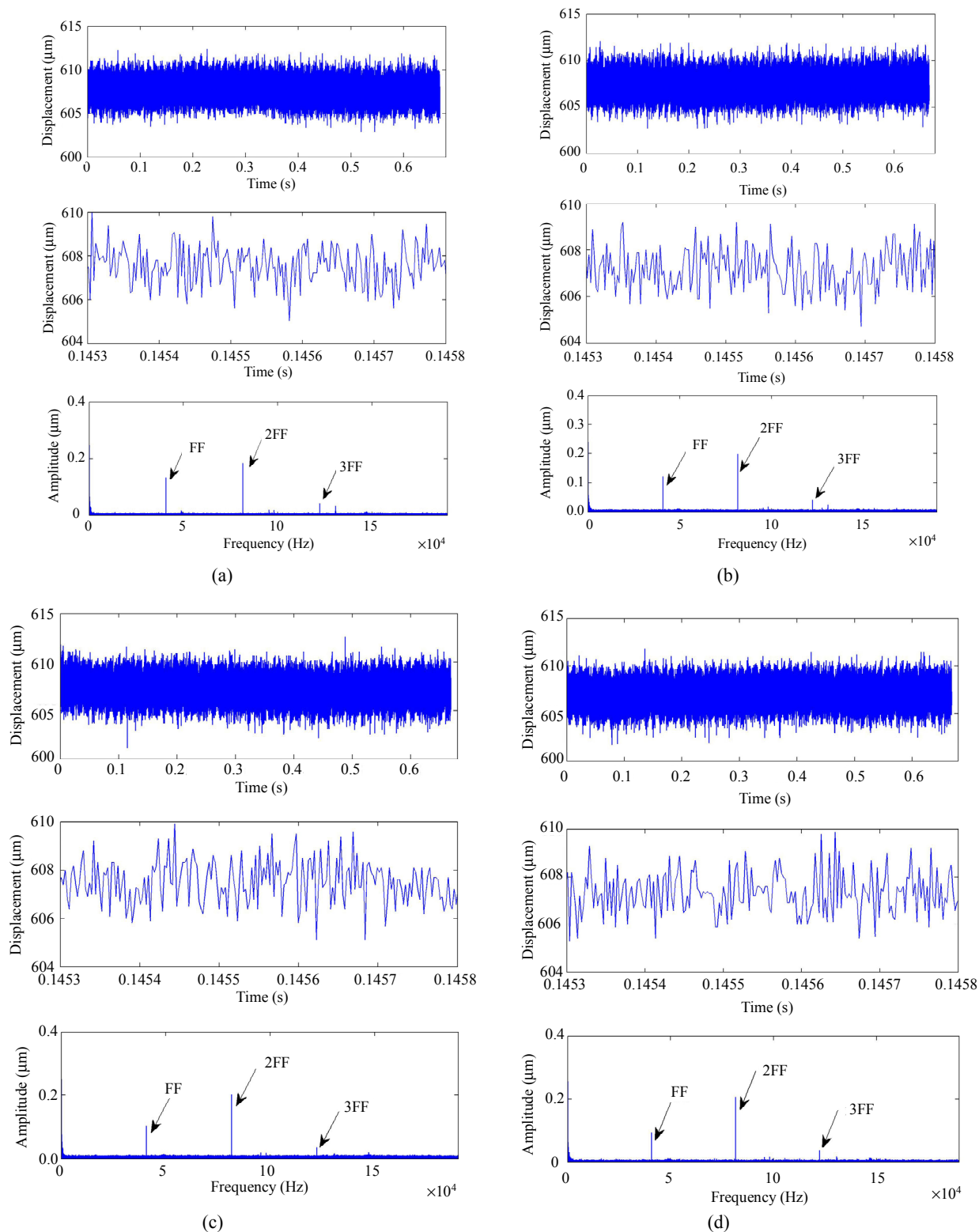


Fig. 6 Vibration displacement during the gather time of 0 s – 0.68 s and 0.1453 s – 0.1458 s and the frequency-spectrum curve of the measurement points: (a) 1#, (b) 2#, (c) 3#, and (d) 4#.

To clearly observe the vibration displacement, the local vibration displacement between 0.1453 s and 0.1458 s is extracted, from which we can find 4 measurement points vibrate inconsistently. But the measurement points vibrate at the same frequency including FF (40 kHz), 2FF (80 kHz), and 3FF (120 kHz), which are approximately agreement with that obtained by the model and proves the validation of the model.

To explore the advantages of the model, the comparative analysis between the results obtained by the model in this work and by that in [7] is carried out. Two models are calculated based on the parameters in this work, and the corresponding results are shown in Fig. 7.

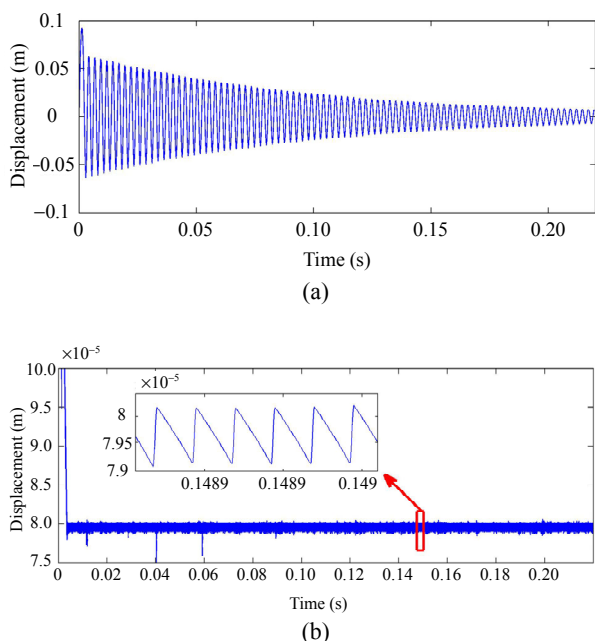


Fig. 7 Vibration displacement of the specimen: (a) obtained by the model in [7] and (b) obtained by the model in this work.

As known in Fig. 7, the response obtained with the model in [7] is gradually damped and indicates that only transient responses are obtained by the model. Comparatively, the vibration obtained by our model is a steady response excited by the ultrasonic gun, which demonstrates the model in this work can ensure the heating efficiency induced by the vibration of the specimen and improve the detection capability. In fact, the ultrasonic gun is continuously

used to excite the specimen, and the collected vibration is the steady response of the specimen. Additionally, our model is to reveal the high order harmonics in the vibrothermography test, which is not observed in [7]. And such phenomenon indicates that our model is closer to the practical equipment than that in [7]. In this case, our model is apparently more reasonable than that in [7].

4. Conclusions

Involving all the contacts in the vibrothermography test, a “double-mass-three-spring” model for analyzing the vibration characteristic is established and solved. The obtained results show that the ultrasonic gun vibrates only at the fundamental frequency while the specimen vibrates at multi-frequencies, which is validated by the experimental results. Compared with the model in [7], the model proposed in this work reveals the high order harmonics in the vibrothermography test and makes the specimen conduct the steady vibration, which indicates the model is closer to the practical equipment and can ensure the heating efficiency induced by the vibration of the specimen to improve the detection capability. Anyone can apply this model within the NDT (Nondestructive Testing)-world and profit from it.

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